Radio Design 101 Appendix B - RF Impedance Conversions

Slides downloaded from: <u>https://ecefiles.org/rf-design/</u> Companion video at: <u>https://www.youtube.com/watch?v=vO-AJjIX7a4</u>

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This video covers series to parallel impedance conversion, its use in matching networks, and in designing and measuring practical RF circuits. Example applications include understanding impedance values shown by RF test equipment and circuit simulations. In addition, an RF cascode amplifier is used to illustrate issues with real-world inductors, oscilloscope probes, and matching to complex impedance values.



$$R_{p} = (1 + q^{2})R_{s}$$
$$X_{p} = (1 + \frac{1}{q^{2}})X_{s}$$
where $q = \frac{X_{s}}{R_{s}} = \frac{R_{p}}{X_{p}}$



Radio Design 101 Appendix B

RF Impedance Conversions

for Matching, Amplifiers, Simulation, and Measurements





Applications



Series to Parallel Impedance Conversion

Matching Networks & Amplifier Design

Lots more !

Background



Associated website: <u>https://ecefiles.org/</u>

R L C Impedances

Z = R + jX



Real-World Components at RF

Ideal

Real-World (Simplified Models)







Series Loss Resistance Parallel Loss Resistance

Theorem

At a specific frequency, an impedance Z = R + jXcan be realized in a series form or a parallel form:



NOTE: <u>At the specific frequency (say f_o)</u>, these two realizations are *equivalent* – they will yield the same circuit behavior and can be swapped to make circuit analysis/design/production easier/cheaper ...

(Constructive) **Proof**

Series form is trivial: $R + jX = R_s + jX_s$

Parallel form is <u>messy</u>: $R + jX = R_p \parallel jX_p$

$$R_p \parallel jX_p = \frac{(R_p)(jX_p)}{(R_p + jX_p)} = \frac{(R_p)(jX_p)}{(R_p + jX_p)} \frac{(R_p - jX_p)}{(R_p - jX_p)} = \frac{R_p^2(jX_p) + R_p(X_p^2)}{R_p^2 + X_p^2} = R_p \frac{X_p^2}{R_p^2 + X_p^2} + jX_p \frac{R_p^2}{R_p^2 + X_p^2}$$

So, $R + jX = R_s + jX_s = R_p \frac{X_p^2}{R_p^2 + X_p^2} + jX_p \frac{R_p^2}{R_p^2 + X_p^2}$

And, hence...

$$R_{s} = R_{p} \frac{X_{p}^{2}}{R_{p}^{2} + X_{p}^{2}} \qquad X_{s} = X_{p} \frac{R_{p}^{2}}{R_{p}^{2} + X_{p}^{2}}$$

Cleaning up (and solving for R_p, X_p)

An

Define a quality factor
$$q = \frac{R_p}{X_p}$$

Then

$$= R_p \frac{X_p^2}{R_p^2 + X_p^2} \left(\frac{\frac{1}{X_p^2}}{\frac{1}{X_p^2}}\right) = R_p \frac{1}{q^2 + 1}$$

$$X_{s} = X_{p} \frac{R_{p}^{2}}{R_{p}^{2} + X_{p}^{2}} \left(\frac{1/X_{p}^{2}}{1/X_{p}^{2}}\right) = X_{p} \frac{q^{2}}{q^{2} + 1}$$

Re-arranging yields ...

 R_{\bullet}

$$R_p = (1+q^2)R_s$$
$$X_p = \frac{q^2+1}{q^2}X_s = (1+\frac{1}{q^2})X_s$$

NOTE: It can also be shown that

$$q = \frac{X_s}{R_s}$$

The proof is left as an exercise for the reader ;-)



- 1. Convert series-form simulation or measurement results to parallel form, to better understand effects on circuit
- 2. Derive / understand impedance matching networks
- 3. Quantify real-world inductor and capacitor parasitics
- 4. Design RF amplifiers !

Convert Series Z to Parallel Form



Measured loading of probe <u>at 100 MHz</u> in series form is:

 $Z_{meas} = 48 - j \ 161$ $q = \frac{161}{48} = 3.35$

 $R_p = (1 + 3.35^2)48 = 588!$ (not 10 M)

$$X_p = \left(1 + \frac{1}{3.35^2}\right) 161 = 175$$

$$C_p = \frac{1}{2\pi f X_p} = 9.1 pF$$
 (a bit less than 15p)

Real-World Inductors



Assume L2, C2+ C_{cb} resonate at 100 MHz,

Suppose R2 = 3K and gm=20mA/V

Then, for matched load $(R'_L = 3K)$, we *should* have R = 1.5K and Av = -30 V/V (29.5 dB) *if* L2 is ideal

Practical inductors have Q from 10 to 100, depending on size, construction.

Suppose L2 is 100 nH ($X_L = 63 Ohms @ 100 MHz$)

If Q of L2 is 10, then $R_s = 6.3$, and $R_p = (1 + 10^2)6.3 = 636 \ Ohms$ and *R* falls to 447 and Av falls to 8.9 V/V (19 dB) !

L Matching Network Design





L Matching Network Design

Basic L network:



Design Procedure:

- Given a desired transformation $R1 \leftrightarrow R2$, equate the lowest resistance (call it R1) with the "series side" of the matching network. I.e. R1 = Rs and R2 = Rp.
- Compute the required q value from:

$$q = \sqrt{\frac{R_p}{R_s}} - 1$$

· Compute the series reactance from:*

 $X_s = \pm qR_s$

• Compute the parallel reactance from:*

 $X_p = \mp \frac{1+q^2}{q^2} X_s = \mp \frac{R_p}{q}$

· Convert to capacitance and inductance values using

 $L = \frac{X_L}{2\pi f}$ and $C = \frac{1}{2\pi f X_c}$

* If one component is selected to be capacitive, then the other must be inductive. The choice of which type to use for a particular side of the network depends on other circuit design considerations. For example, the choice:

- will determine whether a "lowpass" or "highpass" response is present outside the primary matching frequency.
- may affect the bias circuit design, or
- may make it possible to save on the number of circuit components by careful combinations of the functions of components such as the matching capacitor and a required AC output coupling capacitor.

Matching Network Example



Design/verify output MN for converting 50 Ohm load to $R'_L = 3K$ at 100 MHz

$$q = \sqrt{\frac{R_p}{R_s}} - 1 = \sqrt{\frac{3K}{50}} - 1 = 7.68$$
$$X_s = q(50) = 384 \qquad \Rightarrow C_s = \frac{1}{2\pi(100E6)(384)} = 4.15pR$$
$$X_p = (3K)/q = 391 \qquad \Rightarrow L_p = \frac{391}{2\pi(100E6)} = 622nR$$





Matching to Complex Zin





At 100 MHz,

$$Z_{in} = R_s + j X_s = 65 - j 360$$
$$q = \frac{360}{65} = 5.54$$
$$R_p = (1 + q^2) R_s = 2.06K$$
$$X_p = \frac{(1+q^2)}{q^2} X_s = 372$$
$$C_p = \frac{1}{2\pi (100E6)372} = 4.28 \text{ pF}$$

Full RF Amp Simulation @



NOTE: We should probably delete R2 here. Why?

For More Information



For Even More Information

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This site is dedicated to educational materials on <u>Radio Frequency</u> <u>Circuits and Systems</u>, and <u>Fundamentals of Electrical and Computer</u> <u>Engineering</u>, and is associated with the <u>MegawattKS channel on</u> <u>YouTube</u>.



ECE Fundamentals





https://ecefiles.org/ece-topics/

https://ecefiles.org/rf-design/

Select a link above for videos, slides, and related information, or select one of the items below to jump to a specific topic:

- Antennas and Propagation Video Series
- Slides for Antennas and Propagation Video Series
- <u>Radio Design 101 Video Series</u>
- Slides for Radio Design 101 Videos
- <u>RF Test Equipment</u>
- <u>RF Circuit Prototyping Boards</u>
- University-level Radio Design Course Materials
- Fundamentals and Additional "ECE Topics"

Thanks for visiting ! Please check back periodically for updates.

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RF Circuits Course Notes





Designing and Building Transmitters and Receivers in a Single Semester

This page was created to document <u>a senior design course</u> taught by the author for 20 years at Kansas State University. It is related to the <u>"Radio Design 101" series of videos on YouTube</u>, but goes into more depth (at the expense of being less polished in presentation)

Lectures and Class Handouts

Each link below leads to lecture notes (hand written and a bit rough) plus course handouts (typed and much nicer) on the associated topic.

- Syllabus, Parts List, and Typical Assignments
- Prototyping Boards
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- <u>Course Introduction</u>
- <u>Electronic Amplifier Design</u>
- Transistors at RF
- <u>Resonant Circuits</u>
- Component Parasitics
- Impedance Matching and Power Gain
- Transmission Lines and Smith Charts
- Two Port Linear Circuit Modeling and S-Parameters
- RF Test Equipment
- Oscillators, Varactors, and VCOs plus Crystals and TCXOs
- Transmitters, Antennas, FCC Rules, and Midterm Exam
- Mixers and Frequency Downconversion
- Toroids, Transformers, and Cores
- Filters
- IF Amp, Demod, and Audio Amp
- Final Receiver Assembly
- <u>Student Notes and Circuit/Measurement Pics</u>

Thanks For Watching !